

PRELIMINARY REPORT OF SUBSURFACE EXPLORATION AND GEOTECHNICAL ENGINEERING EVALUATION

US HIGHWAY 221 MEGA-SITE LAURENS COUNTY, SOUTH CAROLINA

Prepared For

LAURENS COUNTY DEVELOPMENT CORPORATION



June 28, 2007



ECS Carolinas, LLP Geotechnical • Construction Materials • Environmental

June 28, 2007

Mr. Marvin Moss Laurens County Development Corporation C/O Laurens County Chamber of Commerce P.O. Box 248 Laurens, South Carolina 29360

Reference: Report of Preliminary Geotechnical Study US Highway 221 Mega-Site Laurens County, South Carolina ECS Project No: 14-4123

Dear Mr. Moss:

As authorized by your acceptance of our proposal number 14-4902-P, dated April 12, 2007, ECS Carolinas, LLP (ECS) has completed the preliminary subsurface exploration for the above referenced project. This report contains the results of our subsurface exploration, as well as our preliminary recommendations regarding the geotechnical design and construction aspects of the project.

We appreciate the opportunity to be of service to you during this early phase of the project and look forward to our continued involvement during the final design and construction phases. If you have any questions concerning the information and recommendations presented in this report, or if we can be of further assistance, please do not hesitate to contact us.

Sincerely, ECS CAROLINAS, LLP represented by;

Kathleen D. Hodson, E.I. Staff Engineer

1/28/05 Stephen J. Geiger, P.E. Principal Engineer ~11111111110 ECS

CAROLINAS, LLP

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1.0 PROJECT INFORMATION

This report contains the results of our preliminary subsurface exploration for the approximately 1,381 acre Mega-Site located near the southwestern quadrant of the intersection of US Highway 221 and US Interstate 385 in Laurens County, South Carolina. Overall site topography is moderate and variable, with elevations interpreted from the USGS quadrangle ranging from approximately 550 to 700 feet MSL. Localized drainage features, indicated as blue lines on the most recent USGS survey, are tributaries of Little River, and generally trend from north to south. Much of the site is wooded or overgrown fields, although, some small abandoned structures were observed on the site. Additionally, a few mobile homes in the northern portion of the site were also observed. The H&H Grading facility is located in the southern portion of the site.

Future construction at the site has not been established at this time. However, we are assuming industrial development that is typical of the South Carolina Upstate. We expect planned construction to likely include moderate to large manufacturing and distribution type facilities and associated infrastructure.

2.0 EXPLORATION PROCEDURES

2.1 Field Exploration

Twenty-seven soil test borings were drilled at the approximate locations shown on the Boring Location Diagram in the Appendix. The borings were strategically positioned in readily accessible areas of the site in order to preclude the need for mechanized clearing and were positioned to provide reasonable coverage of the site. The borings were advanced to depths ranging from 15 to 20 feet below the existing ground surface. The boring locations were established in the field by ECS personnel by estimating distances and angles from existing site features and from referencing the site topography. The boring locations on the Boring Location Diagram in the Appendix should be considered approximate. Individual Boring Logs are also included in the Appendix of this report.

The soil borings were performed using an all-terrain mounted, CME-550 drill rig utilizing continuousflight, hollow-stem augers to advance the boreholes. Drilling fluid was not used in this process. Representative soil samples were obtained by means of the split-barrel sampling procedure in general conformance with ASTM D 1586. In this procedure, a 2-inch O.D., split-barrel sampler is driven into the soil a distance of 18 inches by a 140-pound hammer falling 30 inches. The number of blows required to drive the sampler through a 12-inch interval is termed the Standard Penetration Test (SPT) value and is indicated for each sample on the boring logs. This value can be used as a qualitative indication of the inplace relative density of cohesionless soils. In a less reliable way, it also indicates the consistency of cohesive soils. This indication is qualitative, since many factors can affect the standard penetration resistance value (i.e., differences between drill crews, drill rigs, drilling procedures, and hammer-rodsampler assemblies) and prevent a direct correlation between SPT resistance value, or N-Value, and the consistency or relative density of the tested soil. Spilt-spoon samples were obtained at approximately 2.5foot intervals within the upper 10 feet of the borings and at 5-foot intervals thereafter.

The drilling crew maintained a field log of the soils encountered in the borings. After recovery, each sample was removed from the sampler and visually classified. Representative portions of each sample were then sealed in glass jars and brought to our laboratory in Greenville, South Carolina for visual examination by a geotechnical engineer.

2.2 Soil Classification

A geotechnical engineer classified each soil sample on the basis of texture and plasticity in accordance with the Unified Soil Classification System (USCS). The group symbol for each soil type is indicated in parentheses following the soil description on the Boring Logs. A brief explanation of the USCS is included in the Appendix of this report.

3.0 SITE AND SUBSURFACE CONDITIONS

3.1 Site Observations

The site is located in the southwestern quadrant of the intersection of US Highway 221 and US Interstate 385 in Laurens County, South Carolina. The subject site consists of multiple parcels comprising approximately 1,381 acres. Much of the site is wooded or overgrown fields. However, some small abandoned structures were observed on the site, in addition to a few mobile homes in the northern portion of the site. The H&H Grading facility is located in the southern portion of the site. Localized drainage features, tributaries of Little River, traverse the site and generally trend from the north to south. Overall site topography is moderate and variable, with elevations interpreted from the USGS quadrangle ranging from approximately 550 to 700 feet above MSL.

3.2 Area Geology

The project site is located in the Piedmont Physiographic Province of South Carolina. The soils in the Piedmont Province typically consist of residuum (weathered in-place soils) derived from the parent bedrock which typically consists of amphibolite-grade metamorphic rocks. The residuum can be found in both weathered and unweathered states. Although the surficial materials normally retain the structure of the underlying parent bedrock, they typically have a much lower density and exhibit strengths and engineering properties of soil. In a mature weathering profile of the Piedmont Province, the soils are generally found to be finer grained near the surface where more extensive weathering has occurred. With increased depth, the particle size becomes more granular and gradually changes to partially weathered rock and ultimately to unweathered bedrock. The mineral composition of the parent rock and the environment in which the weathering occurs is largely responsible for the residual soil's engineering properties.

It is important to note the presence of alluvial soils at the site. Areas adjacent to rivers (e.g. Little River, etc.), stream and creeks are often underlain by alluvial (water deposited) soils that can extend to significant depths depending on the topography of the area prior to deposition. Alluvium consists of unconsolidated clay, silt, sand, gravel and cobbles deposited by water. It is not uncommon for alluvial soils to contain organic inclusions.

3.3 Subsurface Conditions

Generally, the soil test borings encountered natural residual soils from the ground surface to their termination depths of 15 feet to 20 feet below the existing ground surface, with the exceptions of Borings B-6, B-8, B-10, B-12, B-19 and B-27. Boring B-6, B-8, and B-19 initially encountered 2 to 6 inches of topsoil which was underlain by natural residual soils. It is important to note the lack of topsoil in the remaining borings was due to their location along existing dirt roadways. Borings B-10, B-12, and B-27 encountered alluvial soils from the ground surface to depths ranging from 8 feet to the termination depth of 15 feet below the existing ground surface. The residual soils typically classified as stiff to hard fine sandy silt (ML) and very loose to dense silty fine sand (SM). The standard penetration resistance (N-values) recorded in the residual soils typically classified as firm to very stiff fine sandy silt and clayey silt (ML) and very loose to medium dense silty fine sand (SM), with N-values ranging from 6 to 20 bpf.

Of particular interest are the deposits of alluvial (water deposited) materials encountered within Borings B-10, B-12, and B-27. The alluvial soils are typically fine to course grained soils characterized as having relatively low strength and high in-situ moisture content which are deposited in low-lying areas associated with former or existing drainage features. The thickness of the alluvial deposits is often highly variable as the result of the depositional environment in which the soils were deposited.

Partially Weathered Rock (PWR), which is very hard soil with N-values of 100 or greater, was encountered in test borings B-11 and B-26, from approximate depths of $11\frac{1}{2}$ feet and $3\frac{1}{2}$ feet below the ground surface to their termination depths, respectively.

Groundwater was observed in Borings B-12 and B-27 at depths approximately 8.8 feet and 4.8 feet below the prevailing ground surface at the time of drilling, respectively. Some of the boreholes caved above their terminations depths and groundwater observations could not be made below the caved depths upon the completion of the field drilling activities. Groundwater levels should be expected to fluctuate as a result of seasonal variations in precipitation, surface water run-off characteristics, and other factors. In general, the highest groundwater levels typically occur in late winter and spring, while the lowest levels typically occur in late summer and fall.

On sites where there is significant topographic relief and evidence of natural drainage features is evident, wet weather springs are often encountered. It would not be unusual to find such conditions in the immediate vicinity of the drainage features or in areas where the subsurface conditions would promote spring activity (more permeable soils overlying less permeable soils).

The above paragraphs provide a general summary of the subsurface conditions encountered at the site at the time of our exploration. The Boring Logs included in the Appendix contain detailed information regarding the subsurface conditions encountered at each boring location. These Boring Logs represent our visual classification of the samples retrieved during the field exploration. The stratification lines on the Boring Logs designate approximate boundaries between various subsurface strata. The actual in-situ transitions are expected to be more gradual.

4.0 CONCLUSIONS AND PRELIMINARY RECOMMENDATIONS

Based on the subsurface conditions encountered within the test borings and our past experience with similar subsurface conditions and construction, the natural residual soils encountered in the borings typically appear suitable for support of lightly to moderately loaded structures on conventional shallow foundations. Foundations may also be supported on properly placed and compacted engineered fill. Furthermore, properly prepared residual soils and properly placed and compacted engineered fill should typically be suitable for support of conventional slabs-on-grade and pavements. These items are discussed in more detail in the following sections of this report. Final subsurface explorations and engineering assessments should be performed for the individual facilities to be located in the proposed industrial park.

Alluvial soils were encountered at Borings B-10, B-12, and B-27. These areas are associated with natural drainage features. The development of these portions of the site will be complicated by the presence of these compressible soils, because if not completely removed or stabilized, new grade supported improvements (e.g. pavements, sidewalks, utilities, shallow foundations, slabs-on-grade, etc.) constructed over alluvial deposits could experience undesirable settlement. If alluvial soils are encountered within planned building footprints, they should be removed entirely, and replaced with new engineered fill. Within paved areas, unstable alluvial soils should be removed or stabilized in place, if possible. In no case shall alluvial soils remain within 4 feet of the finished subgrade elevation beneath paved surfaces. Localized undercutting, stabilization with geo-synthetics and/or surge stone, or some combination of these methods would typically be considered appropriate. Construction phase dewatering

may be necessary to perform site work activities in areas underlain by the alluvial deposits.

4.1 Foundations and Slabs

Based on the preliminary information from borings, it appears that the residual soils at the site should typically be capable of supporting conventional shallow foundations designed for bearing pressures in the range of 3,000 to 5,000 pounds per square foot (psf). Structures supported by new engineered fill may utilize shallow foundations preparations for a maximum net allowable bearing pressure of 3,000 psf. The net allowable bearing pressure refers to that pressure which may be transmitted to the foundation bearing soils in excess of the final minimum surrounding overburden pressure.

Properly prepared residual soils and engineered fill should also be satisfactory for supporting concrete slabs-on-grade. Our preliminary findings indicate that a modulus of subgrade reaction (k_s) in the range of 100 to 150 pounds per cubic inch (pci) will likely be available provided the subgrades are properly prepared.

Slabs-on-grade should be constructed in a manner so as to be structurally independent of the column and wall footings in order to reduce the risk of unwanted differential settlement-related distress. Depending upon the time between achieving the final grades and the time to begin slab construction for the structures, a structural slab may be necessary if sufficient settlement of the underlying alluvial soils and overlying fill mass has not occurred.

4.2 Engineered Fill

Fill placed beneath foundations, slabs or pavements should consist of engineered fill. In general, engineered fill should consist of an approved material, free of organic matter and debris and cobbles greater

than 4 inches, and have a Liquid Limit (LL) and Plasticity Index (PI) less than 40 and 20, respectively. We also recommend that all fills within structural areas have a standard Proctor maximum dry density (ASTM D 698) of at least 90 pounds per cubic foot (pcf). Unsuitable fill materials include topsoil, alluvial soils, organic materials (OH, OL), and high plasticity clays and silts (CH, MH).

It appears that natural residual on-site soils similar to those sampled in the test borings will generally be suitable for re-use as engineered fill. Groundwater was observed in Borings B-12 and B-27 at depths of 8.8 and 4.8 feet at the time of drilling. It may not be practical to use soils obtained from below the groundwater level due to the work involved with drying these materials. Moisture conditioning of the on-site soils during placement as fill to facilitate proper compaction.

Some of the soils sampled in the borings contained moderate percentages of mica. These materials are often troublesome when used for engineered fill due to difficulties with properly adjusting their moisture content. Furthermore, micaceous soils are very sensitive to disturbance when exposed at subgrade and often exhibit relatively poor pavement support characteristics especially under heavy loaded pavements.

Engineered fill within the building and pavement areas should typically be placed in lifts not exceeding 10 inches in loose lift thickness, be moisture conditioned to within approximately 3 percent of the optimum moisture content and be compacted to a minimum of 95 percent of their standard Proctor maximum dry density as determined in accordance with ASTM D 698. In general, the upper 18 to 24 inches of the fills should be compacted to at least 98 percent of their standard Proctor maximum dry density as determined in accordance their standard Proctor maximum dry density as determined in accordance their standard Proctor maximum dry density as determined in accordance their standard Proctor maximum dry density as determined in accordance their support characteristics under slabs and pavements.

4.3 Pavement Considerations

Properly prepared residual soils and engineered fill should typically be satisfactory for supporting pavements. Based on our past experience, California Bearing Ratio (CBR) values of 4 to 6 can typically be developed for soils similar to those encountered during this study which are properly prepared. CBR tests should be performed during the final subsurface explorations to determine appropriate CBR values for use in pavement design.

4.4 Excavation

Boring B-1 encountered auger refusal at a shallow depth and this suggest that an isolated pinnacle of rock or a resistant large boulder or rock ledge of may be present in at least the northern portion of the site. PWR was encountered in Borings B-11 and B-26 at depths of 11½ feet and 3½ feet below the existing surface, respectively. However, the borings were spaced relatively widely and most were advanced to relatively shallow depths, and it is possible for additional shallow rock, boulders or PWR to be present intermediate of the test borings locations. The potential for encountering rock (or partially weathered rock, which can be difficult to remove from confined excavations) will typically increase with increasing excavation depth. We recommend that rock be defined as follows:

Mass Excavation

Rip Rock - All subsurface materials that cannot be excavated using scrapers, loaders, or bulldozers; and requires pre-loosening with a bulldozer equipped with a single-tooth ripper blade and having a minimum

draw bar pull rating of 56,000 pounds (i.e., Caterpillar D-8K or equivalent), or requires a Caterpillar 977 trackloader or equivalent to achieve excavation.

Blast rock - All subsurface materials that cannot be excavated or pre-loosened with a Caterpillar D-8K, Caterpillar 977, or equivalent equipment, and occupying an original volume of at least one cubic yard.

Trench Excavation

Blast Rock - All subsurface materials that cannot be excavated or pre-loosened with a track-mounted backhoe having a minimum bucket curling force rating of 25,500 pounds (i.e., Caterpillar 225 or equivalent), and occupying an original volume of at least $\frac{1}{2}$ cubic yard.

Additionally, areas of mass excavation, trenches and pits should meet the requirements of the most current Occupational Safety and Health Administration (OSHA) 29 CFR Part 1926, "Occupational Safety and Health Standards-Excavations". Regardless, site safety shall be the responsibility of the contractor and his subcontractors.

There is a potential for encountering groundwater in deeper excavations at the site, and the potential for encountering groundwater is likely the greatest in the vicinity of the creeks and other drainage features. The potential or encountering groundwater and rock will also be increased with increasing excavation depth, and should be further evaluated as the final subsurface explorations for the future developments are performed.

4.5 Other Geotechnical Considerations

Alluvial soils will likely be present adjacent to the existing creeks. Alluvial soils are water deposited materials that are often found in a soft or very loose condition and will tend to settle significantly under loads from structures or fill placed above them. Therefore, developing areas adjacent to the creeks may be more difficult than other areas of the site and require improving subgrade conditions prior to construction.

Soils containing some quantities of mica were occasionally sampled in the test borings. These soils can be relatively weak and easily disturbed, and provide relatively poor subgrade support for heavily loaded slabs and pavements. Micaceous soils may be more suited for placement in deep fill areas.

4.6 Seismic Site Classification

South Carolina has adopted the 2003 Edition of the International Building Code (IBC), and the IBC 2003 requires that a seismic Site Class be assigned for new structures. To determine the site class, the soil profile has to be characterized to a depth of 100 feet. The soil profile in the most of the industrial park site likely classifies as a Site Class C or D.

Once individual structures are sited at the park, a seismic Site Class should be determined for each subdivided parcel. The savings in construction costs between the C and D classifications can be significant. The Site Class can be determined by extending a conventional soil test boring to refusal or a depth of 100 feet and using the N-Value method presented the Section 1615 of the IBC. Although convenient, the N-value method is relatively conservative, especially in the Piedmont residual soils in South Carolina. An alternate method is also presented in Section 1615 of the IBC that uses in-situ measurements

of shear wave velocities. Although this method requires specialized equipment to measure in-situ shear wave velocity, it often results in the determination of a more favorable Site Class and can significantly reduce construction costs. Refraction Microtremor (ReMi) testing or seismic cone penetration testing are economical methods of measuring the shear wave velocity of subsurface materials.

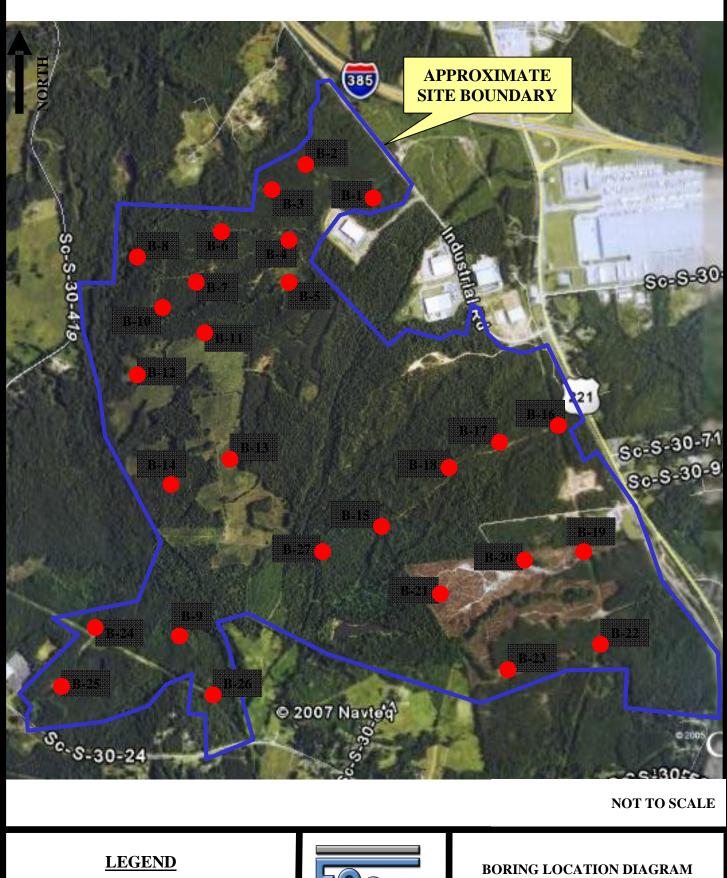
5.0 CLOSING

Our preliminary evaluation of site subsurface conditions has been based on our understanding of the site and project information and from data obtained from the widely spaced test borings. The general subsurface conditions utilized in our preliminary evaluation of the site have been based on interpolation of subsurface data between the borings. The discovery of any site or subsurface conditions during construction which deviate from the data outlined in this exploration should be reported to us for our evaluation. The assessment of site environmental conditions for the presence of pollutants in the soil, rock, and ground water of the site was beyond the scope of this exploration.

Final subsurface explorations and geotechnical engineering assessments should be performed prior to design of all planned construction. The final explorations should be based upon the establishment of final siting and grading requirements for each tract and should concentrate on better defining the potential for encountering rock and shallow groundwater in areas to be excavated. These explorations should also include an evaluation of the seismic Site Class on a per-structure basis.

APPENDIX

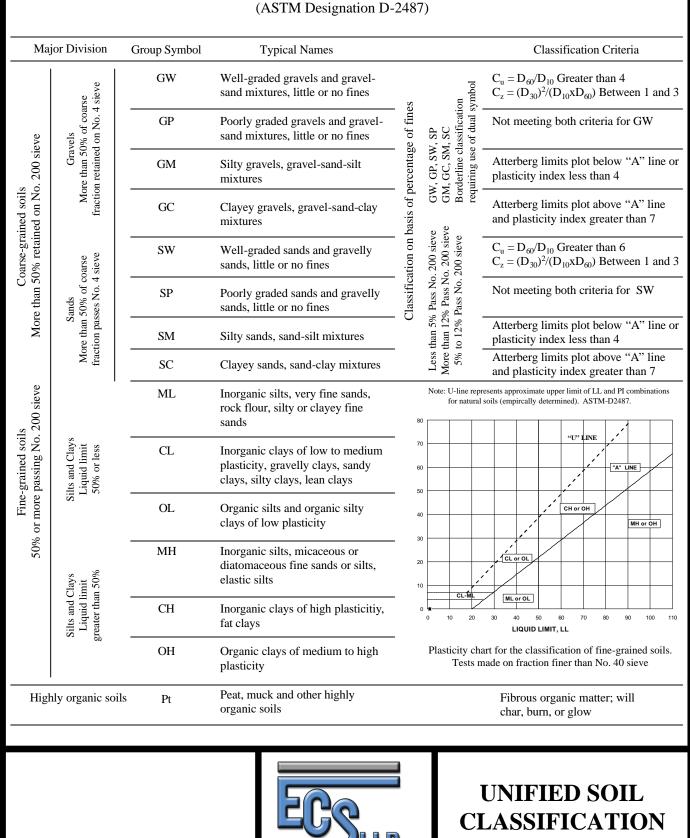
Boring Location Diagram Unified Soil Classification System Reference Notes for Boring Logs Boring Logs B-1 through B-27



B-1 SOIL BORING LOCATION



BORING LOCATION DIAGRAM US HIGHWAY 221 MEGA SITE PRELIMINARY GEOTECH LAURENS, SOUTH CAROLINA ECS PROJECT No. 14-4123



SYSTEM

Unified Soil Classification System (ASTM Designation D-2487)

REFERENCE NOTES FOR BORING LOGS

I. Drilling and Sampling Symbols:

SS:	Split Spoon Sampler	RB:	Rock Bit Drilling
ST:	Shelby Tube Sampler	BS:	Bulk Sample of Cuttings
RC:	Rock Core; NX, BX, AX	PA:	Power Auger (no sample)
PM:	Pressuremeter	HSA:	Hollow Stem Auger
DC:	Dutch Cone Penetrometer	WS:	Wash Sample

Standard Penetration (Blows/Ft) refers to the blows per foot of a 140 lb. hammer falling 30 inches on a 2 inch O.D. split spoon sample, as specified in ASTM D-1586. The blow count is commonly referred to as the N value.

II. Correlation of Penetration Resistances to Soil Properties:

Relative Density	of Cohesionless Soils	Consistency of Cohesive Soils	
<u>SPT-N</u>	Relative Density	<u>SPT-N</u>	Consistency
0 - 4	Very Loose	0 - 2	Very Soft
5 - 10	Loose	3 - 4	Soft
11 - 30	Medium Dense	5 - 8	Firm
31 - 50	Dense	9 - 15	Stiff
51 or more	Very Dense	16 - 30	Very Stiff
		31 - 50	Hard

50 or more

Very Hard

III. Unified Soil Classification Symbols:

GP:	Poorly Graded Gravel	ML:	Low Plasticity Silts
GW:	Well Graded Gravel	MH:	High Plasticity Silts
GM:	Silty Gravel	CL:	Low Plasticity Clays
GC:	Clayey Gravel	CH:	High Plasticity Clays
SP:	Poorly Graded Sands	OL:	Low Plasticity Organics
SW:	Well Graded Sands	OH:	High Plasticity Organics
SM:	Silty Sands	CL - ML:	Dual Classification (Typical)
SC:	Clayey Sands		

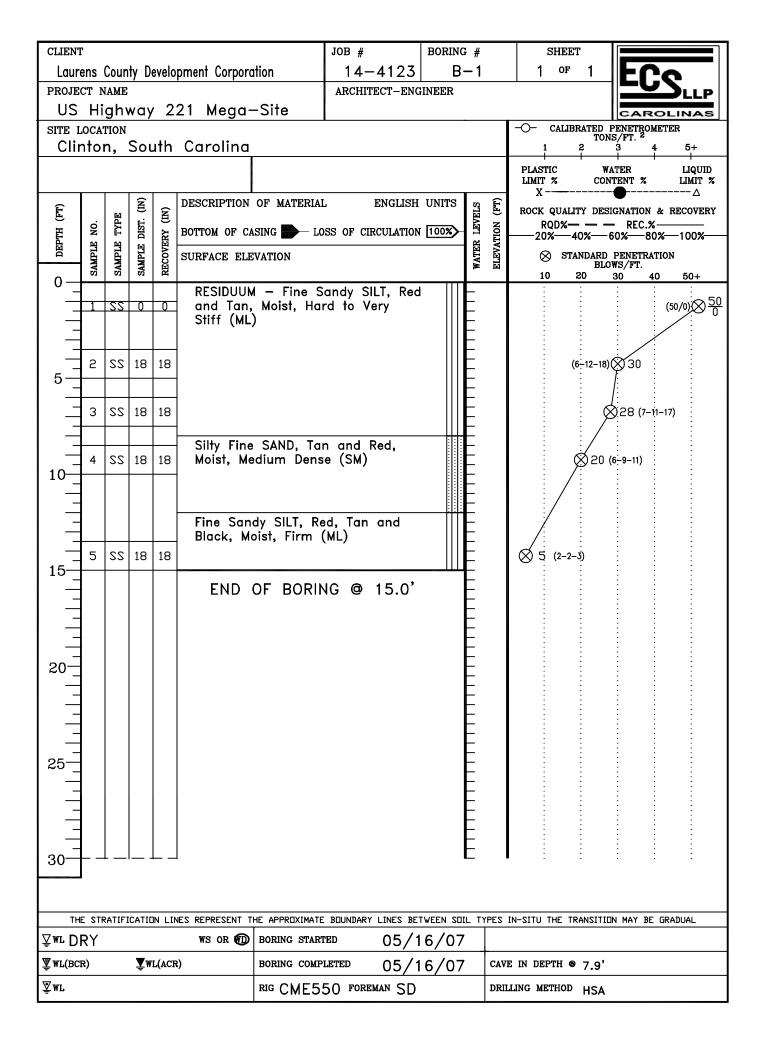
IV. Water Level Measurement Symbols:

WL:	Water Level	BCR:	Before Casing Removal
WS:	While Sampling	ACR:	After Casing Removal
WD:	While Drilling	WCI:	Wet Cave In
		DCI:	Dry Cave In

The water levels are those water levels actually measured in the borehole at the times indicated by the symbol. The measurements are relatively reliable when auguring, without adding fluids, in a granular soil. In clays and plastic silts, the accurate determination of water levels may require several days for the water level to stabilize. In such cases, additional methods of measurement are generally applied.

The elevations indicated on the boring logs should be considered approximate and were not determined using accepted surveying techniques.

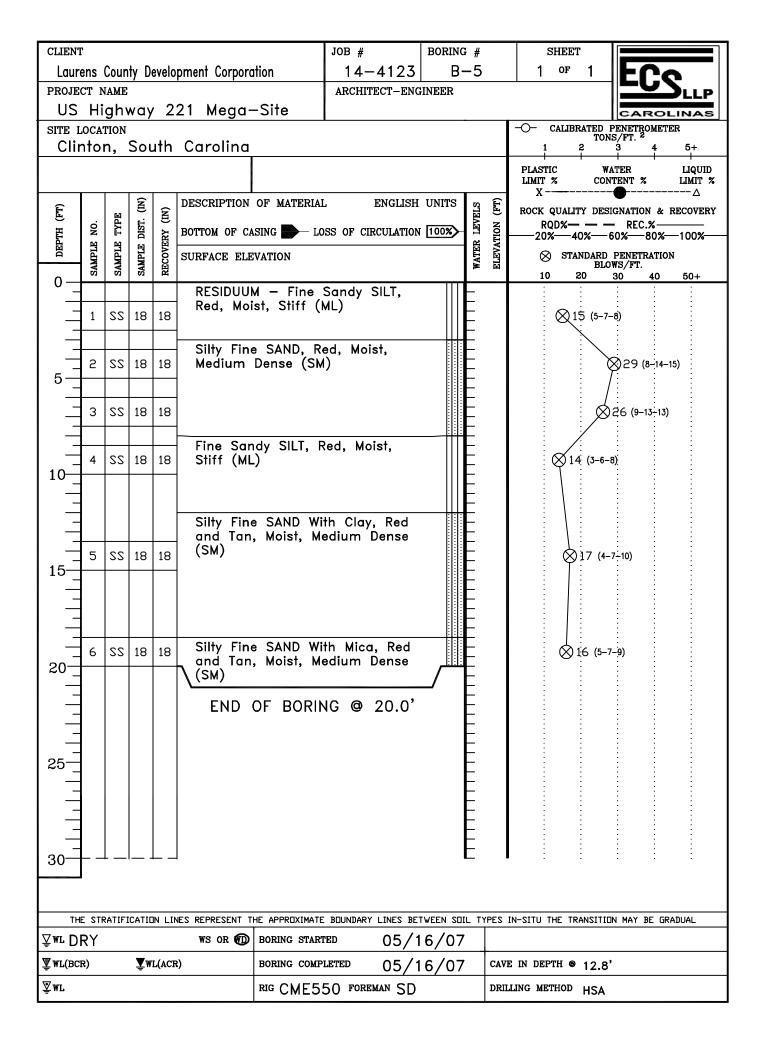


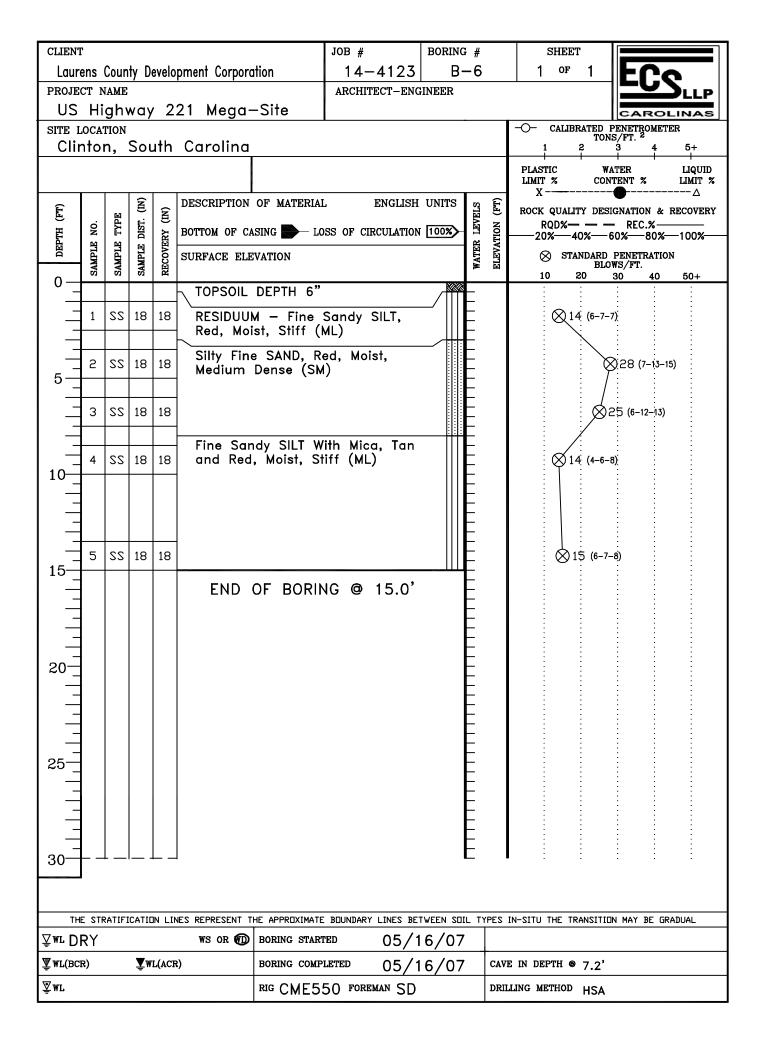


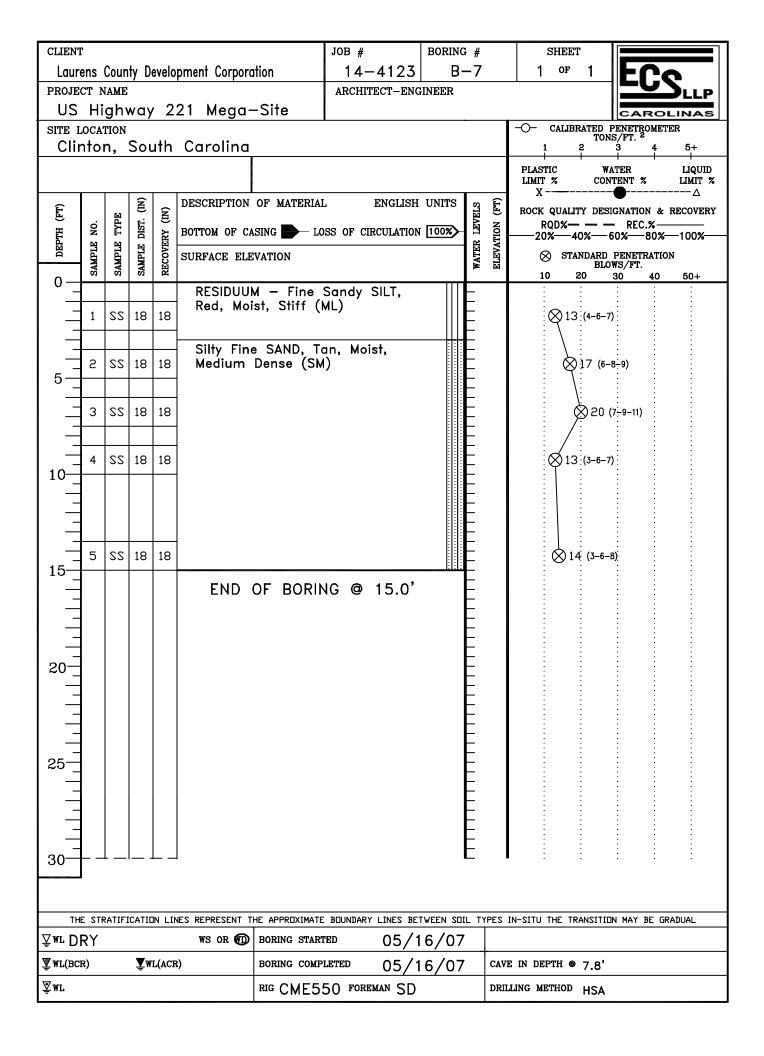
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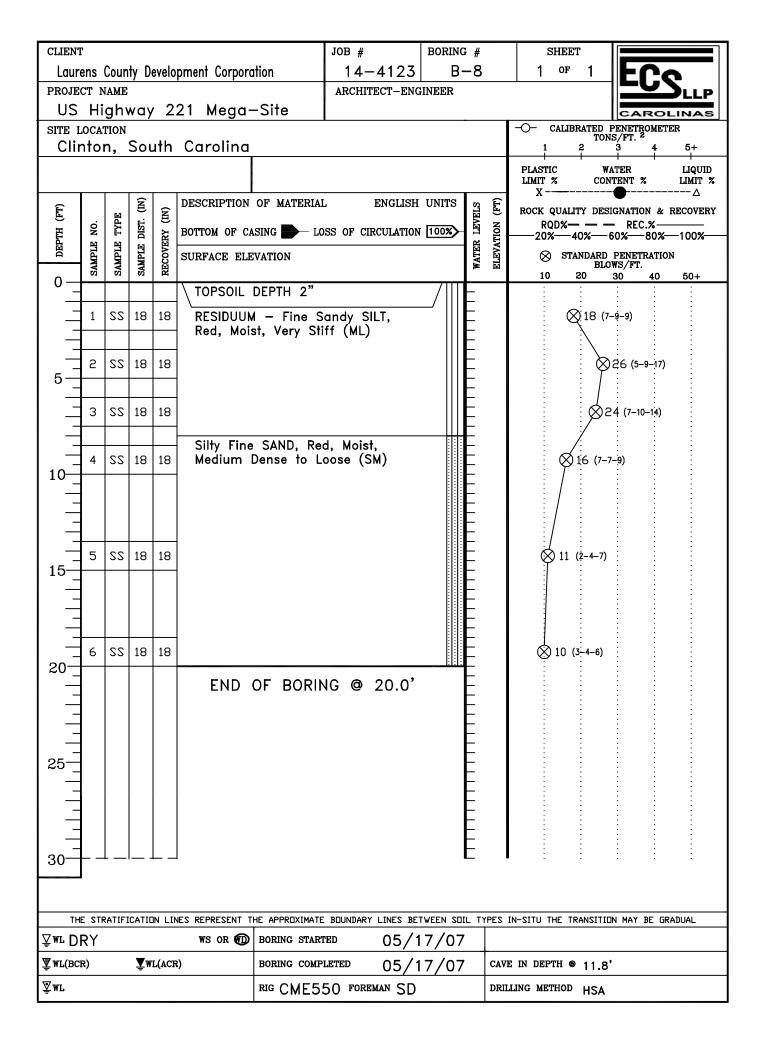
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Ţ wr(BC	R)		Ţw	L(ACF	R) BORING COM		6/07	CAVE	CAVE IN DEPTH @ 10.9'				
Žwl						50 FOREMAN SD	, ·	DRILLING METHOD HSA					
							134						

CLIENT	[JOB #	BORING #		SHEET	
Laur	ens	Coun	ty D	evelo	pment Corporation	14-4123	B-4		1 of 1	ECe
PROJE				_		ARCHITECT-ENG	INEER			
t		-	vay	2	21 Mega-Site		_			CAROLINAS
SITE L Clir			Sοι	ıth	Carolina				-O- CALIBRATED TON 1 2	PENETROMETER S/FT. ² 3 4 5+
										ATER LIQUID ITENT % LIMIT %
(FT)		5	(NI)	(IN)	DESCRIPTION OF MATERIAL	L ENGLISH	UNITS 2	(FT)		IGNATION & RECOVERY
	NO.	TYPE	DIST.		BOTTOM OF CASING 🍆 LC	SS OF CIRCULATION	WITER LEVELS		RQD%— — – 	– REC.%——— 60%——80%——100%——
DEPTH	SAMPLE	SAMPLE	SAMPLE	RECOVERY	SURFACE ELEVATION		ATTER	ELEVATION	STANDARD	PENETRATION
0-	SAM	SAM	SAM	REC			7M	EI	0 BL0 10 20	WS/FT. 30 40 50+
					RESIDUUM - Fine S					
	1	22	18	18	Red, Moist, Stiff (M	L)			⊗14 (4-5-	9)
					Ciller Fine CAND De	d and Tan				
	2	22	18	18	Silty Fine SAND, Re Moist, Medium Dens		E		× 19 (5811)
5_										
	3	52	18	18		al alta la Trava			⊗15 (6-7-	-8)
	-				Silty Fine SAND, Re Moist, Medium Dens	aaisn Tan, e to Loose	E			
			10	10	(SM)		_			
10-	4	22	18	18					× 10 (4-5-5)	
					Silty Fine SAND Witl	n Rock				
					Fragments, Reddish	Tan, Moist,				
	5	22	18	18	Medium Dense (SM)				8)27 (6-11-16)
15					END OF BORIN	NG @ 15.0'				
							F			
							F			
							E			
20_							F			
							F			
							E			
							F			
25							F			
							E			
							F			
							F			
30-							E			
		ATIFI	CATIE	N LIM	ES REPRESENT THE APPROXIMATE			'PES I	N-SITU THE TRANSITIE	IN MAY BE GRADUAL
∑wl DRY ws or € boring starts						ARTED 05/16/07				
WL(BCR) WL(ACR) BORING COM						$\frac{1}{10000000000000000000000000000000000$				
Ž₩L					RIG CME5	50 foreman SD		DRILI	LING METHOD HSA	

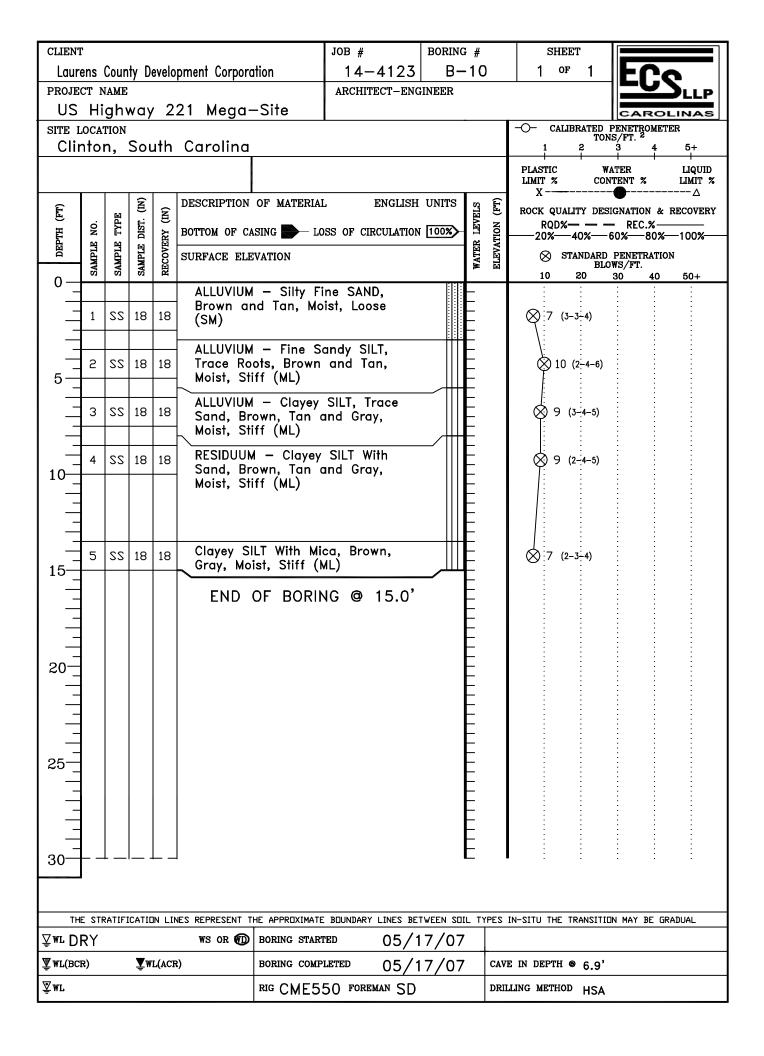






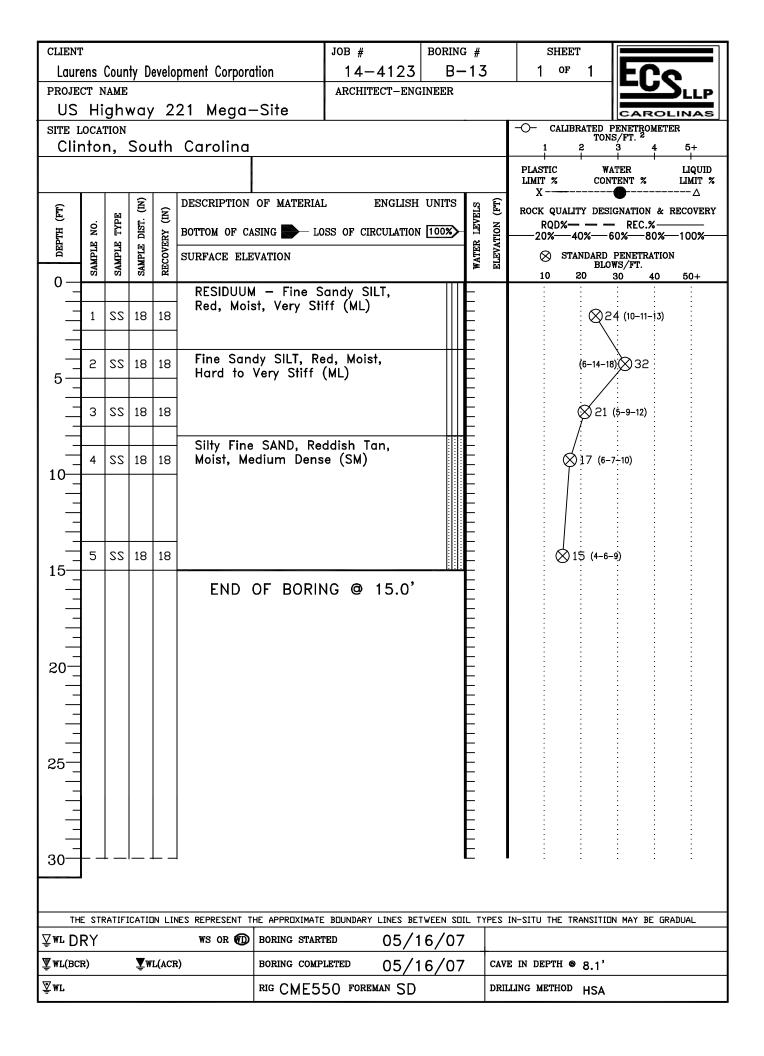


CLIENT	Г						JOB #		BORING	G #		SHEET	
		Coun	ty D	evelo	pment Corpora	ition		4123		-9			
PROJE					II			ECT-ENG					
US	Hi	gh	vay	<u> </u>	21 Mega-	-Site				_		CAROL	
SITE L			~									-O- CALIBRATED PENETROMETER TONS/FT. ²	2
	nto	n,	201	ITN	Carolina						_		5+
		1										PLASTIC WATER LIMIT % CONTENT % X	LIQUID LIMIT % ·····∆
(FT)		臣	(NI) .	(NI)	DESCRIPTION	OF MATERIAI		ENGLISH	UNITS	ELS	(FT)	ROCK QUALITY DESIGNATION & R	ECOVERY
DEPTH	NO.	TYPE	DIST.		BOTTOM OF CA	SING ┣— LO	SS OF CIR	CULATION	100%	WATER LEVELS	ELEVATION	RQD%— — — REC.%— 20%—40%—60%—80%—	100%
DEI	SAMPLE	SAMPLE	SAMPLE	RECOVERY	SURFACE ELE	VATION				ATEF	LEVA	STANDARD PENETRATION BLOWS/FT.	
0_	SA	SA	SA	RE						* '	Ξ	10 20 30 40	50+
					RESIDUUN Red Moi	4 — Fine : st, Stiff (N	Sandy S MI)	SILT,		F			•
	1	22	18	18					F		∞ 12 (3-5-7)	:	
					Silty Fine	SAND, R	ed Mois	s+	E				
	2	SS	18	18	Medium	Dense (SM)	.,	E		20 (4-9-11)	:	
5_										F			•
	3	22	18	18						E		⊗ 19 (6–9–10)	•
									E			•	
	4	52	18	18	Silty Fine	e SAND, To	an and	Red,	E		⊗ 20 (7–11–9)	•	
10-			10	10	Moist, Mo	edium Den	se (SM))	E			:	
										E			•
										E			•
										E			
15-	5	22	18	18						E		(4-6-7)	•
					FND	OF BORIN	1C @	15.0'		E			•
					END	or Borrin		10.0		F			•
										F			•
										E			
20-										F			:
										F			
										E			:
_										F			:
25-										F			•
										F			•
										E			•
										F			•
										F			•
30—	<u> </u>	+			ı					•	J		
	F 970		<u>۲</u>	יז או או				I INES DE	WEEN 07		F 9 1	N-SITU THE TRANSITION MAY BE GRAI	ואוור
Žwr D		<u></u>	UNIL	111 LI	WS OR 1	BORING START					L 3 1	N STIU THE TRANSTITUM MAT BE UKA	JUNL
¥ "" DI V WL(BCI			Ţw	L(ACF		BORING COMP		05/17/07 05/17/07 Cave in Depth © 6.9'					
Ţwr						RIG CME5	50 FOREN	/	e		ORIL	LING METHOD HSA	
L													

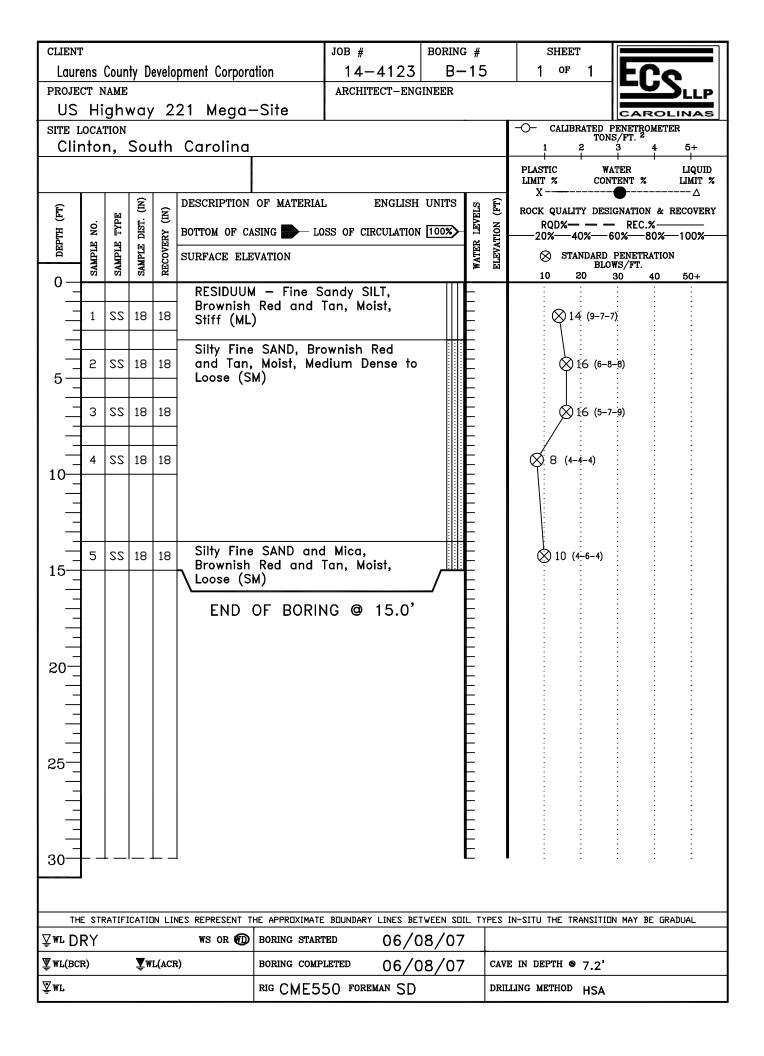


CLIEN	Г						JOB #	BORING	#	SHE	ET		
Laur	ens	Coun	ty D	evelo	pment Corpora	tion	14-4123	В-	11	1 оғ	1	EC	<u>'</u>
PROJE							ARCHITECT-ENG	INEER					
		-	vay	2	21 Mega-	-Site							OLINAS
			501	ith	Carolina						BRATED TON 2	PENETRON	ieter F 5+
		1,	300	1111						Ī			├
										PLASTIC LIMIT %	CON	ATER	LIQUID LIMIT %
Ê			(II)	~	DESCRIPTION	OF MATERIAL	L ENGLISH	UNITS	ELS (FT)				∆ & RECOVERY
H (FT)	NO.	TYPE	DIST.	(III)	BOTTOM OF CA		SS OF CIRCULATION	100%		RQD%-		– REC.%	
DEPTH			LE D	RECOVERY		_			WATER LEVELS ELEVATION (FT	-		60%80 PENETRA)%—100%——
	SAMPLE	SAMPLE	SAMPLE	RECC	SURFACE ELE	VATION			WA' Ele	⊗ S1 10		$\frac{\text{PENETRA}}{30}$ 4	
0_					RESIDUUM	I – Fine S	andy SILT,		_				:
-	1	22	18	18	Red, Mois	st, Stiff (M	L)		-	× () 10	: (4-4-6)		
_									_	Ĭ			
-	2	22	18	18	Silty Fine Moist, Lo	SAND, Tai ose (SM)	n and Red,		-	× 10	: (3 - 4-6)		
5_		33	10	10	- Mol31, E0	030 (311)			-			:	
									_				
-	3	22	18	18					_	⊗ 8 (4	1-4-4) :		
-	1								-				
	4	22	18	18					-	89	(3-4-5)		
¹⁰ _									_		: :		
_					DADTIALLY				_				
-						As: Silty F	ED ROCK - Tine SAND,		_	:	:		
	5	22	12	12	Tan and	Red, Móist	(PWR)		_			(1	1-50∕5.5)⊗ <u>50</u> 5.5
15_									-		:		
-									-	:	:		
_									_				
	6	SS	3	3					_		:		$(50/3)$ $\bigotimes \frac{50}{3}$
20-					51				-	:	÷	:	
-					END (OF BORIN	NG @ 20.0'	E	-		:		
-								F	_		÷		
								F	-				
								E	-				
25									_	•	:		•
								F	-				• • •
								E	-				
-								F	_		:		
30—				L _	l			L	_ 1	:	:	: :	•
			CATI-	NI I T					TYPES		DANSTTE	N NAV DC	GRADUAL
Zwr D		(A) [F]	CALI	JIN L1	WS OR	BORING STAR	MATE BOUNDARY LINES BETWEEN SOIL TYPES IN-SITU THE TRANSITION MAY BE GRADUAL				ULAUUAL		
¥ "" D			▼w	T.(ACF	_	BORING COMP							
¥ #L(BC ŽWL													
Ļ						MG CMED	50 foreman SD			ALING MEIHOL	' HSA		

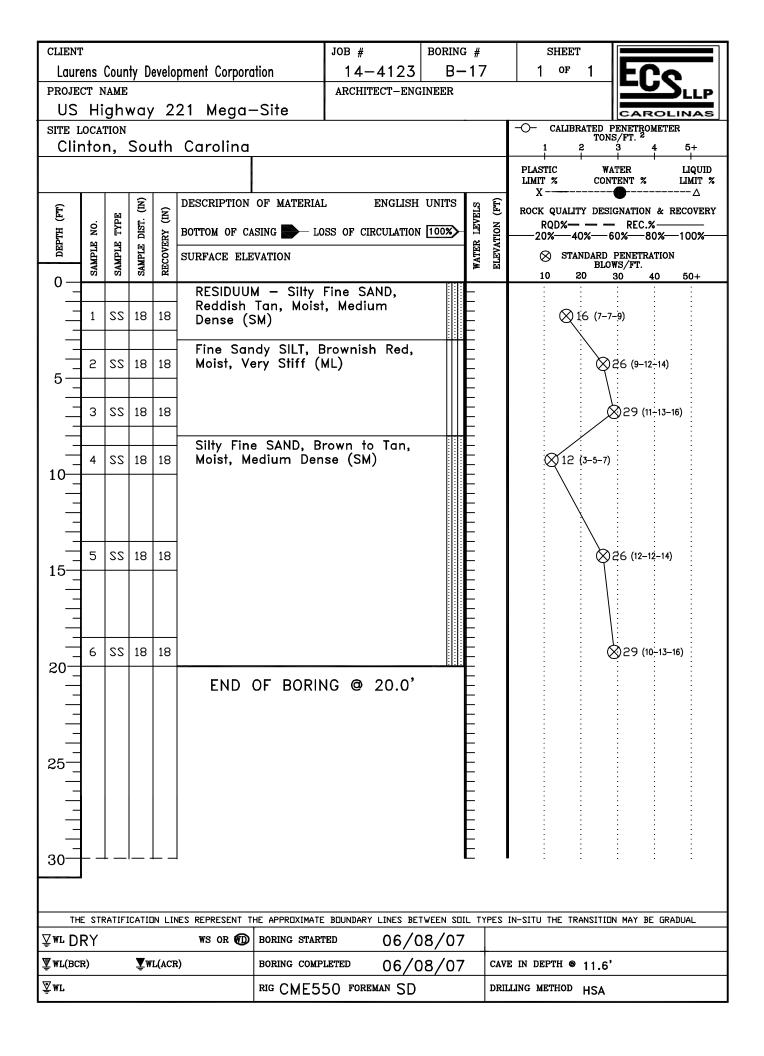
CLIENT							JOB #	BORING	#	SHEET	
Laur	ens	Coun	ty Do	evelo	pment Corpora	tion	14-4123	B— ⁻	12	1 of 1	ECo
PROJE	CT N	AME					ARCHITECT-ENG	INEER			
US	Hi	ghv	vay	<u> </u>	21 Mega-	Site					CAROLINAS
SITE L Clir			Sοι	uth	Carolina					-O- CALIBRATED TO 1 2	PENETROMETER NS/FT. ² 3 4 5+
		,								LIMIT % CO	VATER LIQUID NTENT % LIMIT %
(FT)			(NI)	(II)	DESCRIPTION	OF MATERIAI	E ENGLISH	UNITS	ELS (FT)	X ROCK QUALITY DE	$\neg \bigcirc \neg \bigcirc \neg \neg \neg \land $
DEPTH (F	NO.	TYPE	DIST.		BOTTOM OF CA	SING 📂 LO	SS OF CIRCULATION	100%		RQD%— —	
DEI	SAMPLE	SAMPLE	SAMPLE	RECOVERY	SURFACE ELE	VATION		WATER LEV ELEVATION	BL) PENETRATION OWS/FT.	
0_	01	01	02	I	ALLUVIUM	- Fine Se	andv SILT.		_	10 20	<u>30 40 50+</u> : : :
	1	22	18	18		ots, Reddis			-	⊗ 6 (2-3-3)	
									_		
	2	22	18	18	ALLUVIUM	- Fine Se	andy SILT,	──┼┼╂	-	⊗19	(4-7-12)
5_					Trace Mic	a, Reddish 7 Stiff (M	Brown,		-		
	3	22	18	18	Moisi, vei	y 3111 (M	L)		-	820	(5-9-11)
	4	22	18	18	ALLUVIUM	— Clayey Ice Roots,	SILT With		-	∞16 (4-	7 0)
10			10	10		oist, Very			-		
									-		
									-		
 15—	5	22	18	18					-	⊗ 18 (6-9-9)
					END (OF BORIN	NG @ 15.0'	Ē	-		
								F	-		
								F	-		
20-								E	-		
									-		
								F	-		
25								F	_		
								F	-		
								E	-		
								F	-		
								E			
<u> </u>											
		ATIFI	CATIE	IN LI			BOUNDARY LINES BE		TYPES	IN-SITU THE TRANSIT	ON MAY BE GRADUAL
Σ Σ Σ Ψ Μ Γ Γ Γ			V 147	T (A CT	WS OR 🔞	BORING START					
						BORING COMP		6/07	_	LING METHOD HSA	
÷""						MED:	50 foreman SD			HSA	

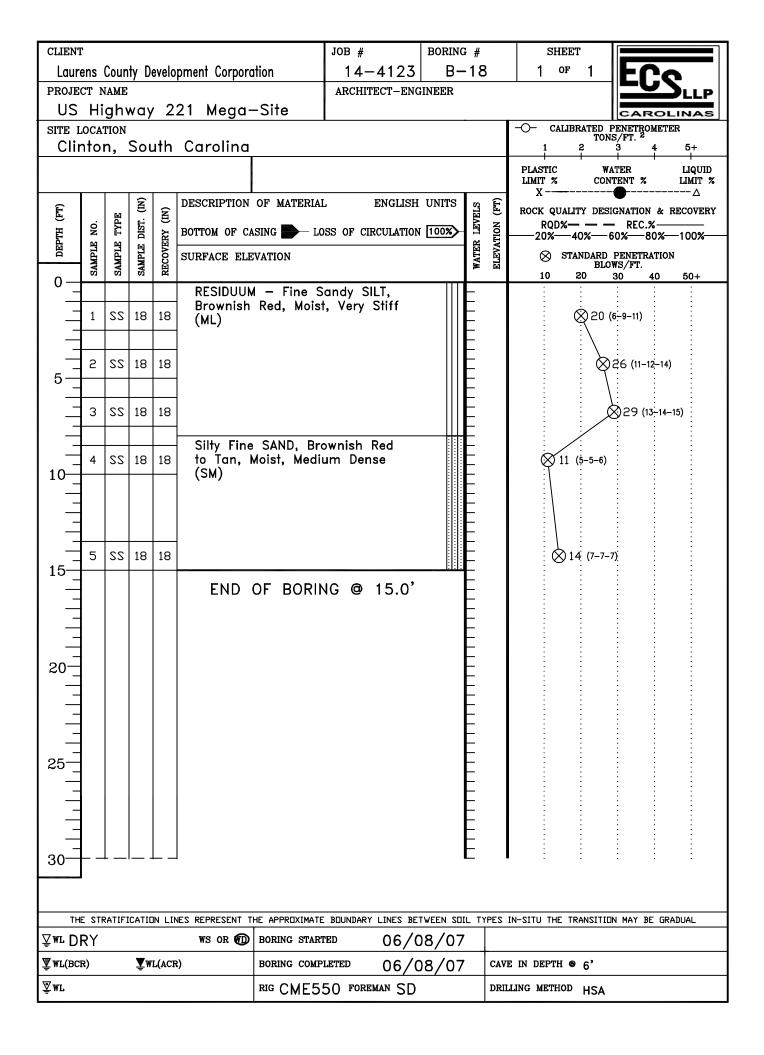


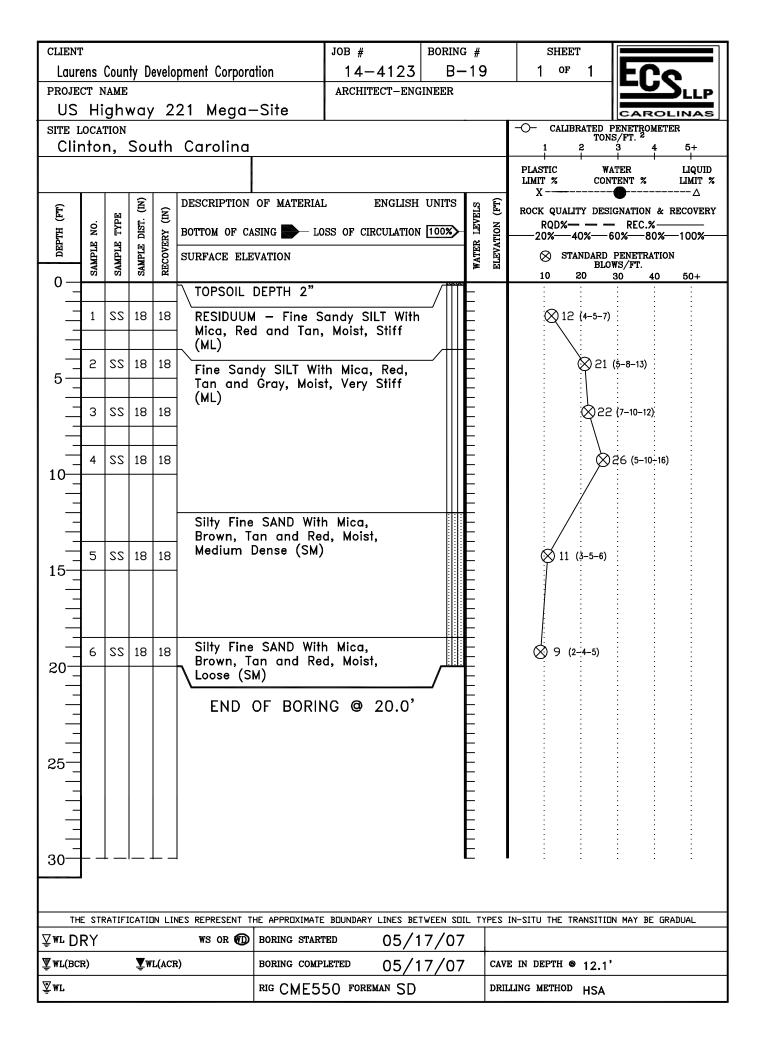
CLIENT	ľ					JOB #	BORING #		SHEET	
Laur	ens	Coun	ty Do	evelo	pment Corporation	14-4123	B-14	1	1 ог 1	ECo
PROJE	CT N	AME				ARCHITECT-ENG	INEER			
US	Hi	ghv	vay	2	21 Mega-Site					CAROLINAS
SITE L			_		•				-O- CALIBRATED	PENETROMETER IS/FT. ²
	ntoi	n, 1	Sοι	ith	Carolina				1 2	3 4 5+
										ATER LIQUID NTENT % LIMIT %
(FT)		м	(NI)	(NI)	DESCRIPTION OF MATERI	AL ENGLISH	UNITS N	(FT)		IGNATION & RECOVERY
	NO.	TYPE	DIST.		BOTTOM OF CASING	OSS OF CIRCULATION	MATER LEVELS		RQD%— — -	– REC.%———— 60%——80%——100%———
DEPTH	SAMPLE	SAMPLE	SAMPLE 1	RECOVERY	SURFACE ELEVATION		TER	ELEVATION	-	PENETRATION
	SAM	SAM	SAMI	REC	SOMPACE ELEVATION		WA	ELI		WS/FT. 30 40 50+
0_					RESIDUUM - Fine	Sandy SILT,				
	1	22	18	18	Trace Roots, Red,	Moist, Stiff		⊗14 (3-6-	8)	
					(ML)					
	_				Silty Fine SAND, T	annish Red,				
5_	2	22	18	18	Moist, Medium Der	se (SM)			⊗19 (5-8-11) : :
<u> </u>										
	3	22	18	18					× 18 (6	-7-11)
	4	22	18	18	Silty Fine SAND, T				⊗ 9 (3-4-5)	
10-					and Black, Moist,	Loose (SM)			Ti i	
_										
15-	5	22	18	18					8 (2-3-5)	
					END OF BOR	NG @ 15.0'	_			
							F			
							F			
							F			
20							E			
							E			
							E			
							F			
							E			
							E			
							F			
30-	L _		— -	L _			E		: :	: : :
		ATIFI	CATIE	IN LII	NES REPRESENT THE APPROXIMA			YPES I	N-SITU THE TRANSITI	IN MAY BE GRADUAL
<u></u> ∑wr D	RY				WS OR (D) BORING STA	rted 05/1	6/07	-		
WL(BCR) WL(ACR) BORING COME						MPLETED $05/16/07$ CAVE IN DEPTH \odot 7'				
Ž₩L						550 foreman SD		DRILLING METHOD HSA		

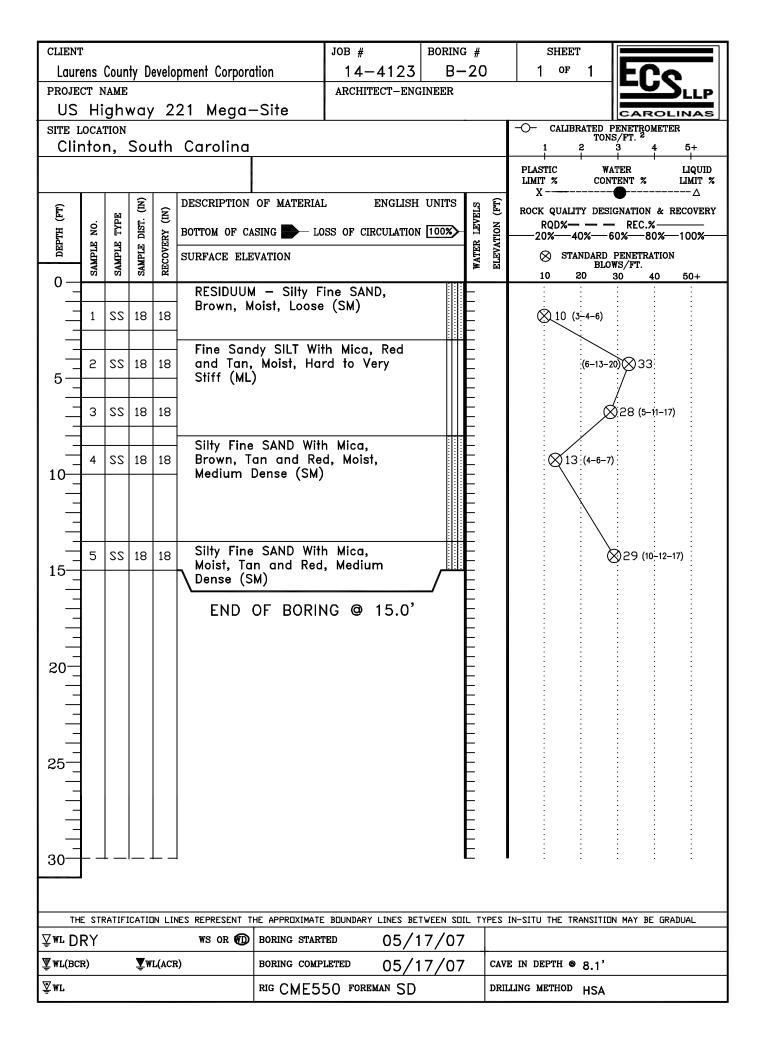


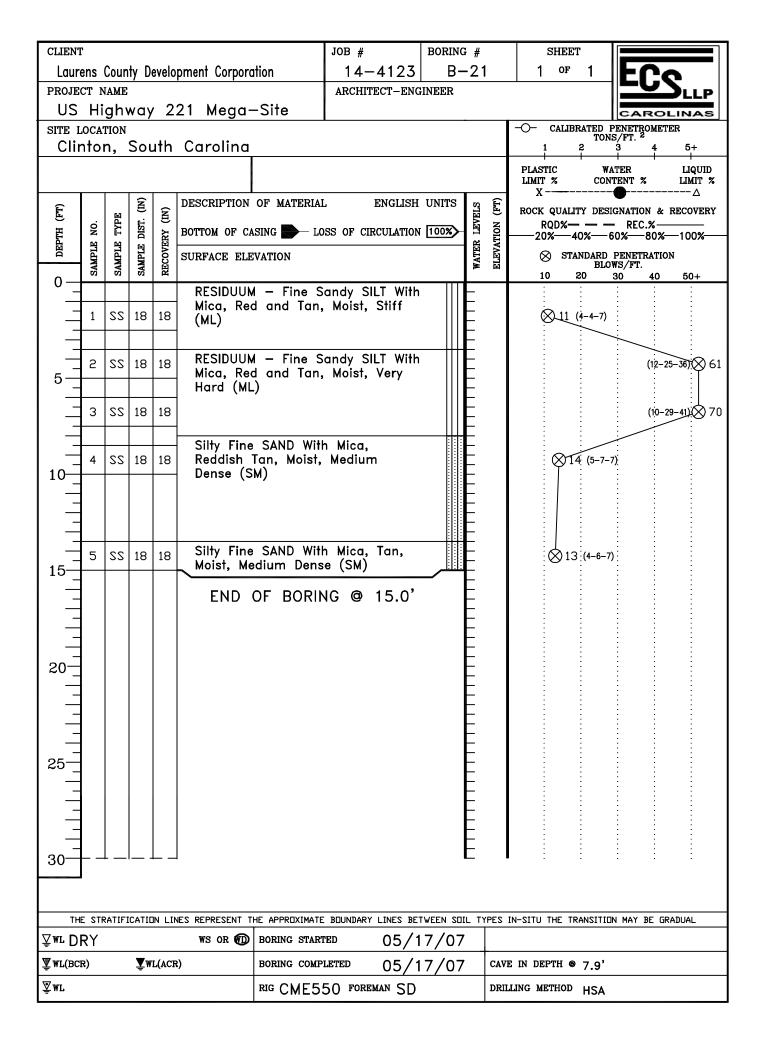
CLIENT	ŗ						JOB #	BORING #		SHI	SHEET				
Laur	ens	Coun	ty D	evelo	pment Corporc	ition	14-4123	B-16	5	1 0	^{off} 1	EC	0		
PROJE	CT N	AME					ARCHITECT-ENG	INEER					JLLP		
		-	vay	2	21 Mega-	-Site							LINAS		
SITE L			_		• ••					-O- CAI	LIBRATED TON	PENETROME S/FT. ²	TER		
	ntoi	า,	Sol	ith	Carolina					1	2	3 4	5+ 		
										PLASTIC LIMIT % X		ATER TENT %	LIQUID LIMIT %		
(FT)			(NI)	(II)	DESCRIPTION	OF MATERIAI	E ENGLISH	UNITS M	(FT)		RECOVERY				
	NO.	TYPE	DIST.		BOTTOM OF CA	SING ┣— LO	SS OF CIRCULATION			RQD	%— — —	- REC.%- 60%			
DEPTH	SAMPLE	SAMPLE	SAMPLE 1	RECOVERY	SURFACE ELE	_		TER	ELEVATION			PENETRATI			
	SAM	SAM	SAMI	REC	SOMPACE ELL	WATION .		M	ELI	BLOWS/FT. 10 20 30 40 50+					
0_					RESIDUU	v – Silty	Fine SAND Wil	h 📗 –		:	:	: :	:		
-	1	22	18	18	Rock Fro	agments, R st. Medium	Reddish Tan ta n Dense (SM)				: ⊗17 (7-	8-9)	:		
	2	22	10	18						:		· · · · · · · · · · · · · · · · · · ·	:		
5_	2	33	18	18								4 (8–12–12)			
										:	÷	3 (8–10–13)	:		
	3	22	18	18											
										:	/:	: :	:		
	4	22	18	18						Ę	ý 15 (4-7-	-8)			
10_												: :			
										÷	:	: :	:		
								E			:				
	_	52	10	10				_			10.15 0 7		:		
15-	5	22	18	18						\otimes	13 (5-6-7				
					END	OF BORIN	NG @ 15.0'	F		:	:	: :	:		
								E							
								E		:	:	: :	:		
								F							
20-								F		:	:	: :	:		
								E							
								E		:	:	: :			
								F							
25								F		:	:	: :	:		
								E		:					
								E		:	:	: :	:		
								F							
								F		:	:	: :	:		
30—					•			•	•	•	·	• •	·		
тн	E STR		CATI	IN I TH	ES REPRESENT T		BOUNDARY LINES BE		YPFS T	N-SITII THE	TRANSITIC	IN MAY BE O	RADUAI		
Žwr D			511		WS OR (D)	BORING START)8/07							
₩ wL(BC			Ţw	L(ACF	2)	BORING COMP)8/07	CAVE	IN DEPTH	6 .4'				
Ž₩L							50 foreman SD		DRIL	LING METHO	DD HSA				

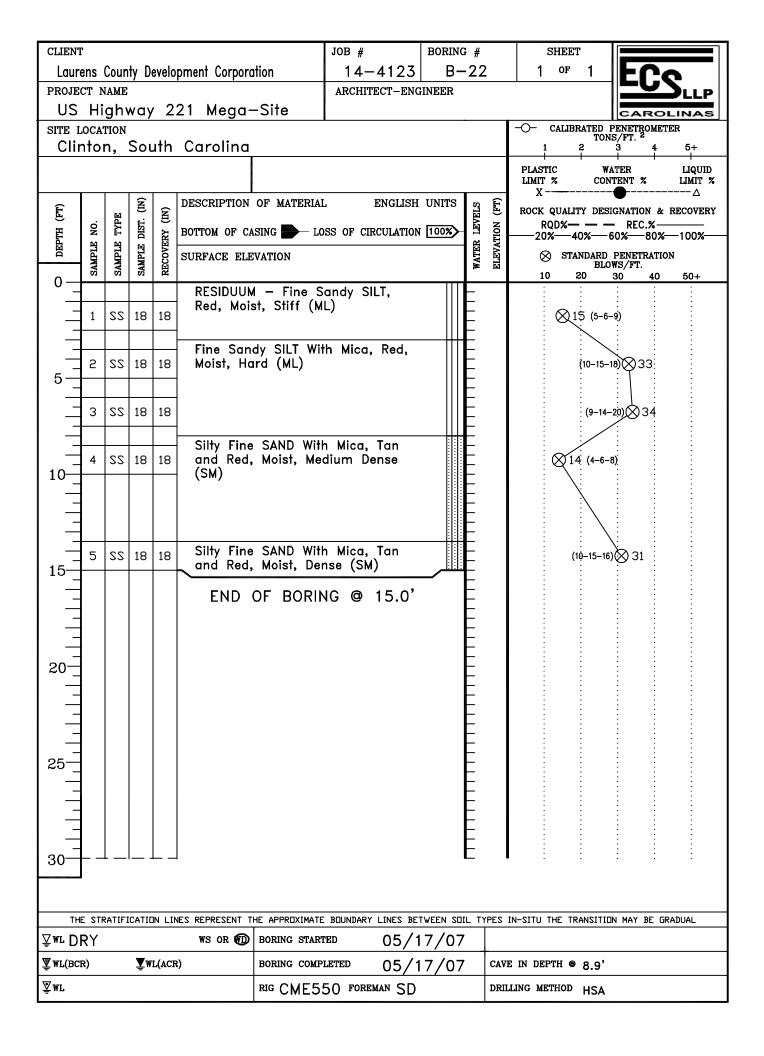












CLIENT	r						JOB #		BORIN	G #	SHEE	т					
		Coun	ty D	evelo	pment Corpora	tion		-4123		-23	1 оғ	1	Fr				
PROJE			-7 -		<u> </u>			ECT-ENG				-		S LLP			
US	Hi	gh	way	· 2	21 Mega-	-Site							CARC	DLINAS			
SITE L Clir			Soi	uth	Carolina					-	-O- CALIB	RATED P TONS 2	ENETROME S/FT. ² 3 4	TER 5+			
		,									PLASTIC LIMIT %		+ + TER TENT %	LIQUID LIMIT %			
			(II)		DESCRIPTION	OF MATERIAI		ENGLISH	UNITS	ELS (FT)	X	(•	Δ			
[(F"T)	NO.	TYPE	dist. (1	(NI)								ROCK QUALITY DESIGNATION & RECOVERY RQD%— — — REC.%———					
DEPTH		E	E DI	RECOVERY			SS OF CL	RCULATION	100%	WATER LEV ELEVATION	20%4			، 100%			
	SAMPLE	SAMPLE	SAMPLE	KECO'	SURFACE ELE	VATION				WAT		BLOV	PENETRATI VS/FT.				
0_	- 01	01	02	-	RESIDUUM	1 - Fine	Sandy		h III		10	20 3 :	<u>30 40</u>	50+ :			
	1	22	18	18	Mica, Red	d and Tar				F	× 10 (· · ·				
_	1	33	10	10	to Very S	Stiff (ML)				F		J=4-0) :					
-										E		:		•			
	2	22	18	18						E	(≫20 (€ /:	5-9-11)	•			
					RESIDUUN	1 - Fine	Sandv	SILT Wi	th III	ŧ		: :	: :	:			
	3	22	18	18	Mica, Tro	ice Roots,	Reda			F	× ×	× 18 (5-9-9)					
					Moist, Ve	ry Stiff (N	ML)			F		:		:			
	4	52	18	18		SAND Wi Moist, Mo				F	×13	: 3 :́(4−5−8)	:	:			
10-					(SM)	MOISI, MO	ealum	Dense		E							
										E		÷		:			
										E		:	: :	:			
										F		:		•			
	5	22	18	18			th Mica, Tan Aedium Dense				i⊗13	3 <u>:</u> (4−6−7)	: :				
15_					and Gray (SM)	r, Moist, N						:	· · ·				
										E							
										E		÷	: :				
	6	52	18	18						F		: [与 (3-6-9	<i>i)</i>				
20-		33	10	10								:0 (0 0 .		•			
					END (OF BORIN	IG @	20.0'		E				•			
										E							
										F		:	: :	:			
										F			· · · · · · · · · · · · · · · · · · ·				
25_										F		:	· · ·				
										F		÷	: :	:			
										E		:	· · ·	•			
										E		:					
30-	L_	$\lfloor -$		L_]					E		:	: :	:			
тн	E STR	RATIFI	CATIC	IN LI	NES REPRESENT TH	E APPROXIMATE	BOUNDARY	LINES BET	WEEN SE	IL TYPES	S IN-SITU THE TR		N MAY BE (GRADUAL			
∑wr D					WS OR 🔞	BORING START		05/1									
			Ţw	L(ACF		BORING COMP	LETED	05/1			VE IN DEPTH ®	E IN DEPTH					
ত RIG CME							50 FORE	MAN SD		DR	ILLING METHOD	HSA					
L																	

CLIENT							JOB #	BORING	#	SHEET					
Laure	ens	Coun	ty D	evelo	pment Corporation		14-4123	B-2	24						
PROJE				_			ARCHITECT-ENC	INEER			LLP				
t		-	vay	2	21 Mega-Si	te					SAL				
SITE L Clir			Sοι	uth	Carolina					-O- CALIBRATED PENETROMETER TONS/FT. 2 1 2 3 4	5+				
										PLASTIC WATER LIQUID LIMIT % CONTENT % LIMIT % X					
(FT)		E	(IN)	(II)	DESCRIPTION OF	MATERIAI	L ENGLISH	UNITS	ELS (FT)	ROCK QUALITY DESIGNATION & REC	_				
DEPTH (E NO.	E TYPE	E DIST.		BOTTOM OF CASING	- LO	SS OF CIRCULATION	100%	WATER LEVELS Elevation (FT	RQD%— — — REC.%—— 20%—40%—60%—80%—1	00%				
	SAMPLE	SAMPLE	SAMPLE	RECOVERY	SURFACE ELEVATI	ON			WAT' Elev	STANDARD PENETRATION BLOWS/FT. 10 20 30 40 50+					
0-					RESIDUUM -	Fine S	andy SILT With		-		:				
	1	22	18	18	Mica, Red, M (ML)	loist, V	ery Stiff		-	×17 (7-8-9)					
									-		:				
	2	22	18	18					-	(6-7-12)	:				
									-		:				
	3	22	18	18					-	8-9-10)	•				
	4	22	18	18	Silty Fine SA Reddish Tan,				-	(\$ 12 (4-6-6)					
10					Dense (SM)				_		:				
									-						
									-						
	5	22	18	18					-	∞ 14 (5-6-8)	· · ·				
					END OF	BORIN	NG @ 15.0'		-		:				
								E	-		:				
									-		:				
20-								E	-						
								F	-						
								E	-		:				
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25-								E	-		:				
25								F	-						
									-						
								F	-						
20-								E	-						
30-															
		RATIFI	CATIE	IN LII		PPROXIMATE			TYPES	N-SITU THE TRANSITION MAY BE GRADU	AL				
Žwr D	RY				WS OR 🔞 BOR	ING STAR	ted 05/1	7/07	_						
₩ WL(BCI	R)		₹w	L(ACF		ING COMP		7/07	_	C IN DEPTH ⊕ 7.6'					
Ÿ₩L					RIG	CME5	50 foreman SD		DRII	LING METHOD HSA					

CLIENT	ſ						JOB #	BORING #			SHEET			
Laur	ens	Coun	ty D	evelo	pment Corpora	ition	14-4123	B-25	5	1	OF	1	EC	0
PROJE	CT N	AME					ARCHITECT-EN	INEER						
US	Hi	gh٧	vay	<u> </u>	21 Mega-	-Site							CAR	OLINAS
SITE I Clir			Sοι	uth	Carolina					-0-		ATED TON 2	PENETROM S/FT. ² 3 4	eter 5+
		-								PLAS' LIMIT			+ + ATER ITENT %	LIQUID LIMIT %
			(II)		DESCRIPTION	OF MATERIAI	L ENGLISH	UNITS 0	£				••	Δ
(FT)	ġ	TYPE		(NI)				VEL	N (FT)				IGNATION	& RECOVERY
DEPTH	E NO.		DIST.	RECOVERY	BOTTOM OF CA	SING 📂 LO	SS OF CIRCULATION		ELEVATION	%—100%——				
DE	SAMPLE	SAMPLE	SAMPLE	SCOV	SURFACE ELE	VATION		WATE	ELEV	Q	3 STAN	NDARD BLO	PENETRAT	'ION
0-	ŝ	ß	7S	R	DECIDIUM	. =:				1	0 2		<u>30 40</u>) 50+ ·
					Mica, Red	1 — Fine S d, Moist, Vo	andy SILT With erv Stiff			:		:	: :	:
	1	22	18	18	(ML)	_,,	.,				(×21	(7–9–12)	:
					Silty Fine	SAND With	n Mica, Tan							
	2	22	18	18	and Red,	Moist, Der	nse to Medium			:		(16–17-	-17) 🛛 34	:
5_					Dense (S	М)						•		
	3	22	18	18								(11-16	: i−i9)⊗35	;
-			10	10						:				' - - -
10-	4	22	18	18						:	\otimes	18 (3	-6-12)	:
¹⁰ _											Ň			
												: \	: :	:
	5	22	18	18								\otimes	: 25 (7-9-16)
15_										:		Ī	: :	:
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20-	6	22	18	18	Sile					:		: Q	<u>)</u> 28 (7−ii	–17) : :
~~_					END (OF BORIN	IG @ 20.0'	F				•		
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тн	E STR	ATIFI	CATIC		ES REPRESENT TI		BOUNDARY LINES BE	TWEEN SOIL T	YPES I	N-SITU	THE TRA	ANSITIC	IN MAY BE	GRADUAL
∑wr D	RY				WS OR 🕅	BORING START	red 05/*	7/07						
Ţ wr(BC	R)		Ţw	L(ACF	:)	BORING COMP		7/07	CAVE	IN DE	PTH 🕲	12.0	•	
Ž₩L						RIG CME5	50 foreman SD		DRIL	LING MI	ETHOD	HSA		

CLIENT							JOB #	BORING #		SHI	EET		
Laurens County Development Corporation PROJECT NAME US Highway 221 Mega-Site SITE LOCATION Clinton, South Carolina							14-4123	B-20	6	1 0	^{of} 1	EC	<u>.</u>
							ARCHITECT-ENC	INEER					
t		-	/ay	2	21 Mega-	-Site							OLINAS
			•		0					-O- CAI	LIBRATED TON	PENETRON	IETER
	iton	I, :	201	ITN	Carolina					1	2	3 4	↓ 5+
										PLASTIC LIMIT %		ATER TENT %	LIQUID LIMIT %
			(N)		DESCRIPTION	OF MATERIAI	ENGLISH	UNITS 🗤	(FT)	X		•	Δ
	ö	YPE	ST. (I					MATER LEVELS	N (F	ROCK QU	& RECOVERY		
EPTH			E DI	/ERY	BOTTOM OF CA	SING 📂 LO	SS OF CIRCULATION	-40%	-60%-80%-100%				
	IAMPI	AMPI	AMPL	ECO	SURFACE ELE	VATION		WATT	ELEVATION	Ŭ		PENETRA WS/FT.	TION
╽╺╶╁	03	00	S	8	RESIDUUM	I – Silty F	ine SAND Red		_	10	20	30 4	0 50+
	1	~~	10	10	and Tan,	Moist, Me	dium Dense			· r	: : : :		
-	1	22	18	18	(SM)					2	015 (7-6	-9)	
-					PARTIALLY	WEATHERI	ED ROCK -						
	2	22	17	17	Sampled	As: Silty F an, Moist (ine SAND,			:	:	(12-	21-50/5) × 50 5
	_				Ked to t	un, moisi ([FWK]				:		50
│ _╂	3	52	4	4						:	:		(50/4) 8 <u>50</u> 4
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	5	33	U										(50/0)⊗ <u>50</u>
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THE	STRA	ATIFIC	CATIO	N LIN	ES REPRESENT T	HE APPROXIMATE	BOUNDARY LINES BE	TWEEN SOIL T	YPES I	N-SITU THE	TRANSITIE	IN MAY BE	GRADUAL
∑w r DF	<u>Y</u>				WS OR 🔞	BORING START	<u>1 05/1</u>	7/07					
₩ WL(BCR	2)		Ţ₩	L(ACF	2)	BORING COMP		7/07	CAVE	IN DEPTH	● 6.3'		
Žwl						RIG CME5	50 foreman SD		DRILI	ING METHO	DD HSA		
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CLIENT	7						JOB #		BORING	G #		SHEE	T						
Laure	ens	Coun	ty D	evelo	pment Corporatio	on		4123		-27		1 оғ	1		C				
PROJE							ARCHITH	CT-ENG	INEER										
t		-	way	2	21 Mega-S	Site				-		0				INAS			
SITE L Clir			Sοι	uth	Carolina							-O- CALIE	BRATED TO 2 	PENETI NS/FT. ³	20METE 4	x 5+ ──			
												PLASTIC LIMIT % X		NATER	%	LIQUID LIMIT %			
(F'T)		M	(NI)	(NI)	DESCRIPTION O	F MATERIAI	1 ،	ENGLISH	UNITS	ELS (pm)	(13)		ITY DE	•	NATION & RECOVERY				
	NO.	TYPE	DIST.		BOTTOM OF CASI	NG ┣— LO	AL ENGLISH UNITS STEAD					RQD%- 20%		— REC -60%—		 _100%			
DEPTH	SAMPLE	SAMPLE	SAMPLE	RECOVERY	SURFACE ELEVA	TION							ANDARI) PENET	RATION				
0-	SAI	SAI	SAL	RE(j≱ ⊑	a	10	20 BL	OWS/FT. 30	40	50+			
Ŭ _					ALLUVIUM - Trace Root	- Fine So s Brown	andy SIL	T,		E			:	:	÷	•			
	1	22	18	18	Moist to Do					F		Ø _. 7 (3-	-3 . -4)	:	÷	•			
					Soft (ML)					E			:	:	÷				
	2	22	18	18						⊻	k	2 (1-1-1)	:						
5_										≚ 				:	:	•			
	3	22	18	18	ALLUVIUM · With Organ	ics, Brow	n and (Gray,		E		♦ 4 (2-1-	3)	:	÷	•			
					_ Moist, Very	Loose (SM)	,.		E				:					
	4	22	18	18	Coarse SAN					E		∑ (2-	4.3)	:	-	-			
10-	4	33	10	10	Rock Fragr Damp, Loo					F			- 4 -5)	:					
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15						F BORIN	പറത	15.0'		E			:	:					
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		ATIFI	CATIE	IN LIN	WS OR D B	APPROXIMATE					S II	N-SILU THE T	KANSIT!	UN MAY	BF CK	JUAL			
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